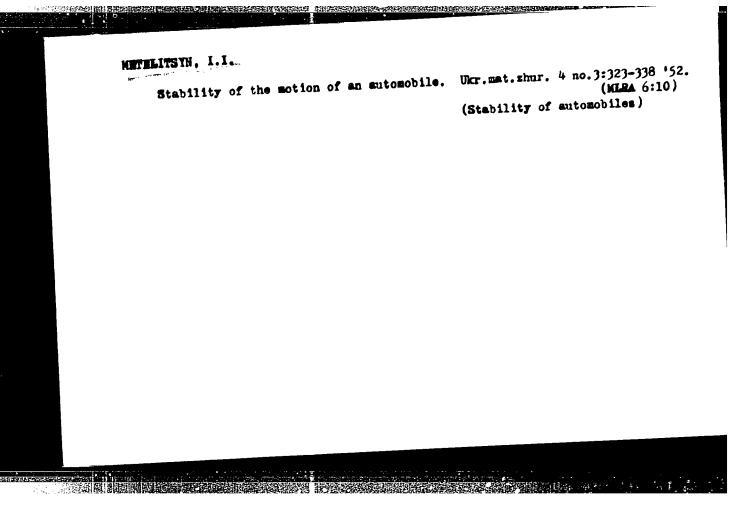
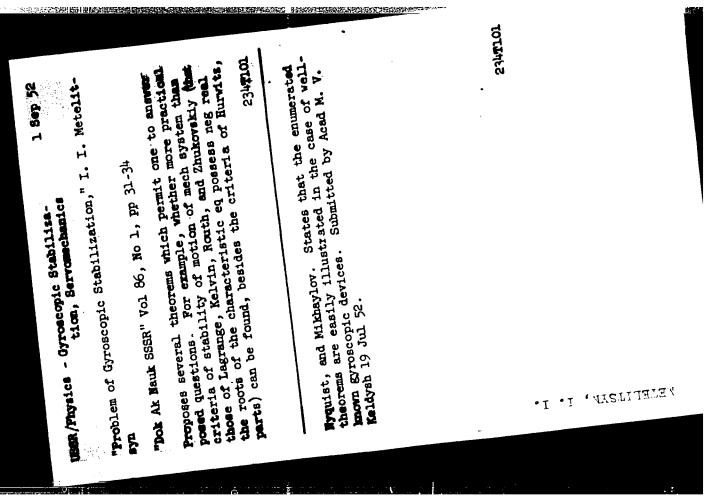
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- 2. USSR (600)
- 4. Physics and Mathematics
- 7. General Problem of Stability of Motion, A. M. Lyapunov (Liapounoff). ("Classics of Natural Science," Moscow-Leningrad, State Technical Press, 1950). Reviewed by I. I. Hetelitsyn, Sov. Kniga No. 7, 1951.

9. Report U-3061, 16 Jan. 1953, Unclassified.



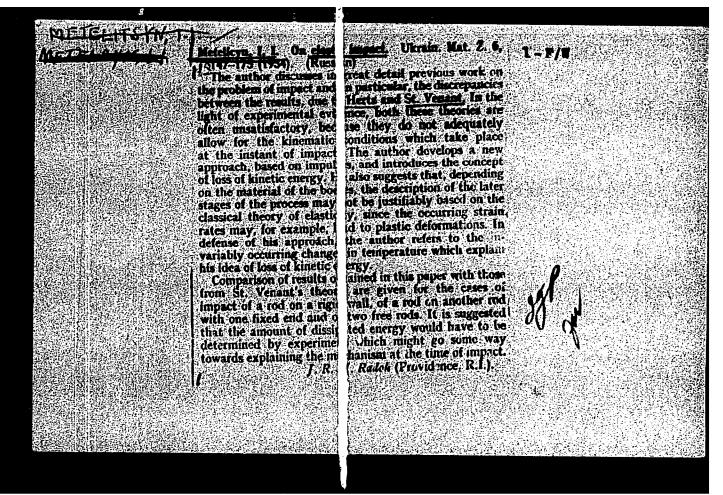
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- 7. Stability of the motion of an automobile; conclusion. Ukr. mat. zhur. 5, No. 1, 1953.

The beginning article appeared in Vol.4, No.3, 1952 of this journal. In this concluding article the author deribes and solves the eqs describing the motion of an automobile with a three-wheel mass, and stablishes the stability of a moving automobile with rigid wheels. Received Aug 50.

9. Monthly List of Russian Accession: Library of Congress, April 1973, Uncl.



METELLIANNE T

AUTHOR: Metelitsyn, I. I. (Moscow)

24-11-14/31

TITLE:

Principle of minimum forcing in the shock theory. (Printsip naimen'shego prinuzhdeniya v teorii udara)

PERIODICAL: Izvestiya Akademii Nauk SSSR, Otdeleniye Tekhnicheskikh Nauk, 1957, No.11, pp. 105-115 (USSR)

ABSTRACT: The Gauss principle is utilised in cases when the movement is studied of a mechanical system with finite forces. For "impact forces" which act for a very short time, the Gauss function 7

forces. For "impact forces" which act for a very short time, the Gauss function Z and the respective variational equation  $\mathbf{\delta Z} = 0$  change. The author attempts to derive the variational equation of the impact theory by the direct method without utilising the Z function. An expression is given for the degree of "forcing" Z' and it is stated that the equation  $\mathbf{\delta Z'} = 0$  enables the determining of the speed occurring during the impact, assuming the initial speeds and impulses as constant. In this case, the fundamental equation of the shock theory can be written in the form expressed by Eq.(1.1), p.106. By making various assumptions on the physical properties of the colliding bodies it is possible to derive from Eq.(1.1) all the known results of the

to derive from Eq.(1.1) all the known results of the shock Card 1/3 theory. The possibility of using the same general approach

Principle of minimum forcing in the shock theory. 24-11-14/31

for solving a variety of differing problems facilitates the solution of new problems which require a new formulation. It is shown in this paper what form the equation  $\mathbf{6Z'} = \mathbf{0}$  assumes for deforming bodies. The equation of the impact theory in generalised coordinates  $q_1, \ldots, q_n$  can be read thus:

$$\frac{\mathbf{T}^{i}}{\mathbf{q}_{k}} = \mathbf{Q}_{k}^{i}$$
 (k = 1, ...,n)

According to the Saint Venant theory, an increase in the modulus of elasticity E and a decrease in density bring about unlimited rise in the stresses under otherwise equal conditions, whilst according to the new theory the stresses rise at first to a certain maximum and then decrease. Therefore, an equal permissible stress for an equal shock load can be obtained in a plate with low as well as with high values of VE/V if a material is chosen which has a higher modulus of elasticity and a lower density. For inelastic bodies the assumed hypotheses and method are applicable, i.e. it can be assumed that for the first phase of the shock the Card 2/3 Eq.(4.1), p.107, expressing the relation between the stress

#### CIA-RDP86-00513R001033710020-4 "APPROVED FOR RELEASE: 07/19/2001

Principle of minimum forcing in the shock theory. 24-11-14/31

> impulses and the components of the deformation speed tensor is applicable and also all the conclusions derived from the variational equation (1.1), p.106, for the case of  $\delta Z' = 0$ . Depending on the intensity of the internal impulses, the first phase may end either with destruction or with a change in the mechanical properties of the colliding bodies or solely with a slight increase in the temperature as a result of loss in the kinetic energy. For the second phase the same equations are applicable which describe the movement of the colliding bodies for finite forces (the equations of the theory of plasticity, of the elastic-viscous body etc.). If for the given problem an accurate or an approximate solution of these equations is found which contains arbitrary constants, the latter can be determined from the condition of the minimum of the "forcing" function.

There are 2 figures and 10 references, 7 of which are

Card 3/3 Slavic.

SUBMITTED: August 22, 1956.

AVAILABLE: Library of Congress.

301/179 - 59-1-1/36

AUTHOR: Metelitsyn, I. I. (Moscow)

Card 1/7

Gyroscopic Systems with a Non-ideal Contact (Giroskopicheskiye sistemy s neideal'nymi svyazyami)

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Mekhanika i mashinostroyeniye, 1959, Nr 1, pp 3-9 (USSR)

ABSTRACT: It can be stated generally that in the case of dry friction the tangent  $F_{s}$ , being a component of a reaction  $R_{s}$ , can be expressed as:

$$|F_g| \leq f |N_g|$$

 $N_{\rm g}$  - normal component of reaction, f - coefficient of friction. Lagrange's equations can be employed for determining the reaction Rg . The case can be shown of a system where one of the elements remains in contact at the supporting point P and N, F', F" are the normal and the two tangent components of the reaction R . The system has n degrees of freedom and its position is determined by the coordinates When the velocity of the point P is v its components along the normal and the tangents of the reaction  $v_n, v_n', v_n''$ 

307/179-59-1-1/36

Gyroscopic Systems with a Non-ideal Contact

can be found from Eq.(1.1) and the work of reaction  $\delta A$  from the expression (1.2). The equation of motion of the system can be shown as Eq.(1.3). When the point P does not slide, then V = 0 and the kinematic relations (1.4) are included in Eq.(1.3). The Eqs.(13) and (14) will give the solution in the ideal conditions, i.e. when the friction is not performing work. In the case of friction in boring and rolling, the corponents of the angle velocity  $\overline{w}$  can be expressed as Eq.(1.5), the forces of resistance by Eq.(1.6) (f<sub>1</sub>, f<sub>2</sub> - coefficients of friction of boring and rolling respectively) and the work as Eq.(1.7). The last equation can be applied in the equation of motion (1.3) as it is shown in Eqs.(2.1),(2.2) and (2.3), where a prinction of coordinate  $q_h$ . From this the following is derived: 1) Reaction of an ideal contact depends only on the instantaneous kinematic state of the system with the active forces and it is not affected by the acceleration  $q_h$ , i.e. reaction can be defined at any instant with no motion considered.

Card 2/7

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Gyroscopic Systems with a Non-Ideal Contact

2) If the forces are those along coordinates, the reaction does not change its value with change of sign of velocities. 3) In the case of cyclic coordinates and appropriate velocity wk (large) being constant, then the terms containing small velocities of the right hand side of Eq.(2.2) can be ignored. Then the reaction of ideal contact can be compared with gyroscopic forces. 4) If there are small vibrations, then the reaction will depend only on the coordinate qh provided the active forces are the functions of coordinates. active forces are the functions of coordinates. All the above is true when the point P does not slide on the resisting surface, i.e. Eq.(2.4) is satisfied. Otherwise (Eq.(2.4) not satisfied) the forces of friction | F | will be equal to All the above fini and Eq.(3.1) takes place while Eq.(1.3) will take the form of Eq.(3.2), so that only Eq.(3.3) will remain of Eq.(1.4). The Eqs.(3.2) and (3.3) sufficiently describe the motion of the system when the condition: Eq. (3.1) are satisfied. Then: (a) the normal of reaction N and forces of friction F' F" are not affected by acceleration, (b) if an additional depends on the coordinates, the normals of the reaction |N| change their value together with the change of Card 3/7 sign of velocities, i.e. force of friction changes its value

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Gyroscopic Systems with a Non-Ideal Contact

and direction, (V) when the coefficient of friction is small, it is possible to predetermine the normals in order to add them to  $Q_h$  (Eqs.(4.1) and (4.5)). In this case, if the vel- $\mathbf{q}_{\mathbf{h}}^{\bullet}$  change their signs, the values of both the ocities reaction and the friction remain the same, (g) in the case of both small vibrations and coefficients of friction, the normals remain constant or depend on the coordinates. (d) if small vibrations are considered in relation to an established motion, then the reaction can be expressed as a linear function of velocity, (e) the sign of  $\varepsilon = \pm 1$  in Eq.(3.2) should be such that |N| > 0 and  $|N| = \varepsilon |N|$ . However, the case may occur when this is not possible (Ref.1). Then the inequality |N| > 0 is upset and  $v_n \neq 0$  (Eq.1.1) and:

$$a_{11}q_1 + \dots + a_{1n}q_h - v_n - \sum_h a_{1h}q_h$$

is obtained instead of Eq. (3.3). Thus the system will break Card 4/7

30**V/179**-59-1-1/36

#### Gyroscopic Systems with a Non-Ideal Contact

contact. As an example, the simple gyroscopic system with the two degrees of freedom and a vertical axis is considered (Fig.1). The normals  $N_1$  and  $N_2$  and their respective forces of friction  $F_1$  and  $F_2$  can be calculated from Eq.(6.1) and the sum of moments equal to  $2 \text{frH} |\alpha|/2 \text{l}$ . This moment has the direction opposite to that of the angular velocity  $\dot{\alpha}$ , therefore it can be expressed as Eq.(6.2). However,  $N_1$  and  $N_2$  will not be equal to each other when the weight of the gyroscope is considered (Eq.6.3). If 1/2 mg 1/2 Ha/1, then the sum of moments will be:

- fmgr (6.4)

but in the case of 1/2 mg<1/2 Ha/1, this moment will be as shown in Eq.(6.2). The moment characteristic is shown in Fig.2. The vibrations of the pendulum with a gyroscope can be calculated from Eqs.(6.5) and (6.6). Different calculations should be performed for the gyroscope with a horizontal axis (Eqs.6.7 and 6.8) (Fig.3). The damping of vibrations in this case will be described by the expression:

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Gyroscopic Systems with a Non-Ideal Contact

$$\frac{d}{dt} (T + V) = -\left|\alpha'\right| fr \sqrt{\frac{mg}{2}}^2 + \left(\frac{H\alpha'}{2}\right)^2 \quad \text{and} \quad T + V > 0$$

and the energy of the system will be decreasing. In order to exclude the gravitational force from the systems, the gyroscope is placed in a rolling frame (Fig.4). Then the reactions  $N_1$  and  $N_2$  and the moment of forces of friction will be:

$$|N_1| = |N_2| = \left|\frac{H\beta}{H\beta}\right|$$
,  $M = -2fr \frac{H\beta}{2t} = -f \frac{r}{t} H\beta$ 

and the equation of motion:

$$B\beta$$
 +  $\frac{\mathbf{t}}{\mathbf{t}}\beta$  =  $H\alpha$ .

If the frame is subjected to a vibrating motion, then the Card 6/7

307/179-59-1-1/36

Gyroscopic Systems with a Non-Ideal Contact

amplitude of the gyroscope will be:

$$\beta_0 = \frac{\alpha_0 \mu / B}{\sqrt{(k^2 - \mu^2) + 4h^2 \mu^2}} \qquad \left(2h = \frac{\text{frH}}{Bl}, k^2 = \frac{C}{B}\right)$$

where  $\alpha_0$  - amplitude and  $\mu$  - frequency (angle) of frame vibrations. There are 4 figures and 2 Soviet references. SUBMITTED: June 27, 1958.

Card 7/7

METELITSYN, Ye., starshiy leytenant

We are always alert. Komm. Vooruzh. Sil 2 no. 19:74-76 0 '61.

(Russia-Armed forces-Political activity)

METELITSINA, G.G., inzh.; PIAKINA, M.E., kand.tekhn.nauk.

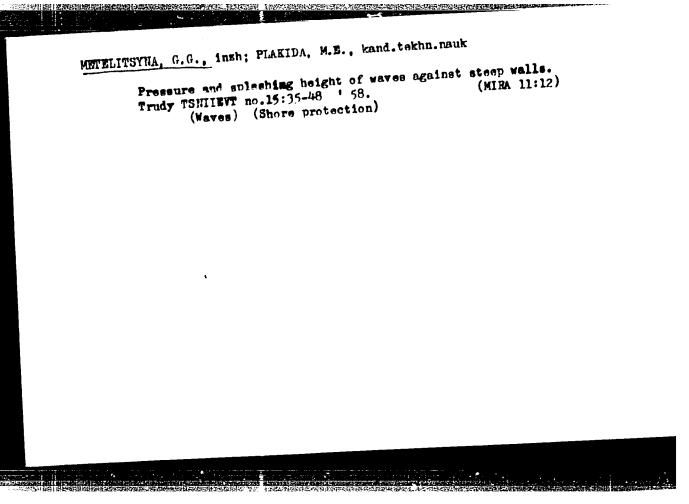
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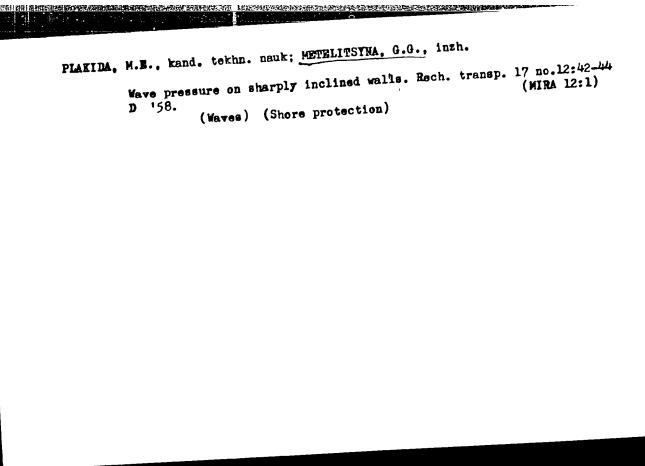
Wave height developed at steep sloping walls. Rech.transp. 16

(MIRA 10:12)

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(Breakwaters) (Waves)





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Hew method of determining wave pressure on vertical reservoir valls. Rech. transp. 18 no.4:41-42 Ap '59.

(Hydrodynamics) (Retaining walls)

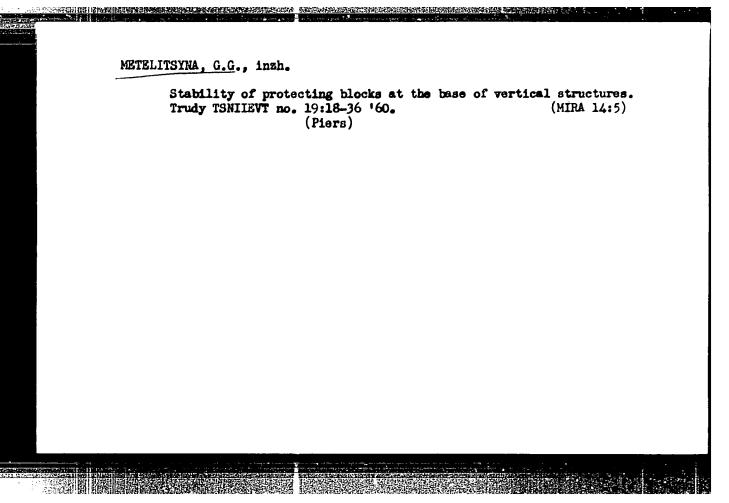
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Wave pressure against steep walls. Trudy TSNIIEVT no. 19:5-17 '60.

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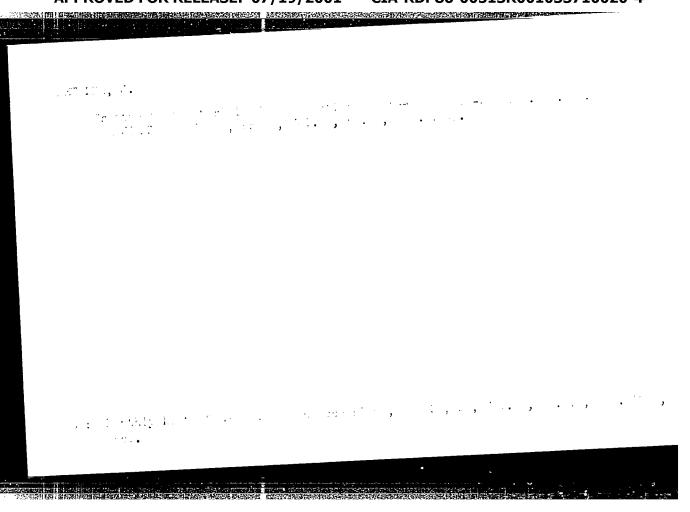
(Waves)

PLAKIDA, M. E.; METELITSYNA, G. G.

"Erosion des fonds de sable devant des murs verticaux et demi-verticaux soumis a l'action de la houle."

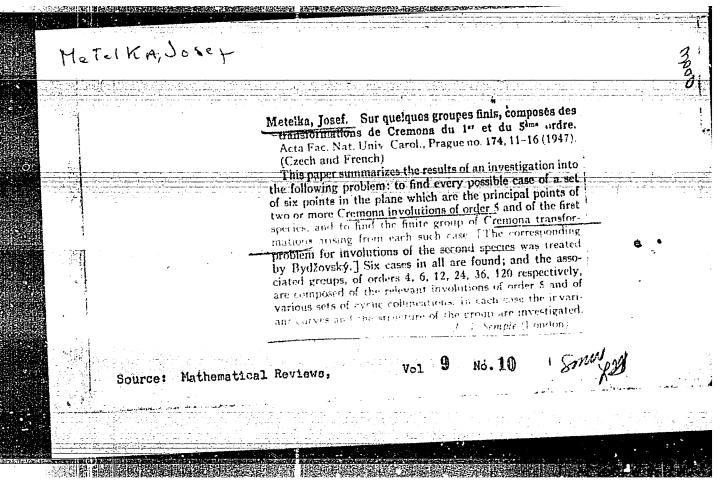
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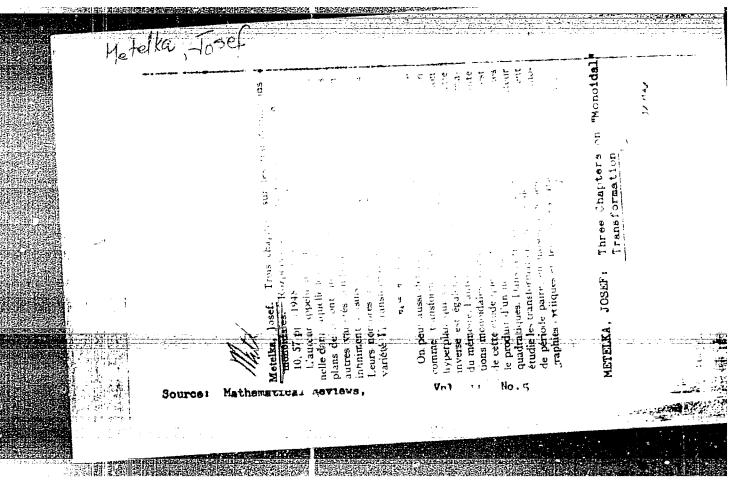


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## METEL KA, Iosif. Remarks on the article of D.D.Mordukhai-Boltovskii "Three-dimen-

sional and four-dimensional analogues of Pascal's theorem. vol.8 no.2(54), 1953, p. 135-138. Usp.mat.nauk 9 no.3:283-284 154. (NEBA 7:10)

(Surfaces) (Nordukhai-Boltovskii, Dmitrii Dmitrievich, 1876-)

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	i report	Ceske Spolethost.  1939 no. 2; MR 7, 390], the author describes a method lot.  1939 no. 2; MR 7, 390], the author describes a method lot.  classifying the fifty-odd known configurations (12, 16 <sub>5</sub> ).  classifying the points from 1 to 12, he considers cases.  Numbering the points from 1 to 12, he considers cases.	
		Numbering the points from 1 to 12, he considered Numbering the points from 1 to 12, he considered where none of the six joins of the four points 9, 10, 11, 12 where none of the six joins of the four points 9, 10, 11, 12 where none of the scheme shows which belongs to the configuration. His scheme shows which other points lie on lines through each of these four. In this manner he distinguishes eight such configurations, four of which are new.  H. S. M. Coxeler.	DM Son

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METELKA, Josef

NAMES DESCRIPTION OF STREET

Alegbra. Pokusne ucebne texty pre 9. roc. vseob. vzdel. skol. l. cast. (Algebra; experimental texts for the 9th grade of schools of general education. Pt. l. a textbook. Tr. from the Czech. illus, notes) Authors: Josef Metalka, Josef Glivicky, and Stanislav Liska. Bratislava, SPN, 1957. 41 p.

Bibliograficky katalog, CSR, Slovenske Khihy, Vol. VIII. 1957. No. 9. p. 276.

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28(2)

PHASE I BOOK EXPLOITATION

CZECH/2001

Metelka, Josef

Kybernetika, myslici stroje (Cybernetics, Electronic Brains) Prague, Orbis, 1957. 65 p. (Series Knihovna československé společnosti pro siření politických a vědeckých znalostí, sv. 151) (Series: Knihovna českoslov-enské společnosti pro šíření politických a vědeckých znalostí. Edice technické

COVERAGE: The pamphlet provides a basic introduction to computing machines, here labeled as "electronic brains". A historic survey precedes the description of the main types of mathematical machines. In this survey the author pays tribute to Norbert Wiener. An explanation of principles underlying the theory and practice of electronic computers follows. The author discusses the two main groups of electronic computing machines, i.e., digital computers and analog machines, and describes the arrangement and functioning of these machines, including the arithmetical operations involved. The "SAPO" memory model machine, the so-called "memory register", mentioned in the text is Czech. A diagram is given. Other examples quoted are non-Czech. The similarity between the brain

Card 1/3

Cybernetics, Electronic Brains CZECH/2001 and these machines, i.e., between digital functioning and the nervous system is reviewed in the last four chapters handling signals and transformation of information. Professor Doctor J. Hrbka, associated with the neurological clinic at Olomonc, is further developing I.V. Pavlov's physiological theories. There are 10 references: 4 Czech , 3 Soviet, 2 English, TABLE OF CONTENTS: None given. The book is divided as follows: Introduction History of Cybernetics 5 Digital Computing 6 Computing Machines 9 Mechanical Counters 12 17 Card 2/3

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<u> </u>	ZECH / 2001
Cybernetics, Electronic Brains  Some Detailed Data on Computers  1. Speed 2. Binary digit 3. Memory	27 27 30 33 37 40
Some Examples of the Use of Electronic Computers  Machine With Conditioned Reflexes  Copying and Analog Operations in Cybernetics	45 48 56
Information Theory Theory of Control and Automation Conclusion AVAILABLE: Library of Congress Card 3/3	60 65 I <b>s/fal</b> <b>8-6-</b> 59

METELKA, J.

"Derivatives in algebra." p. 穷.

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Monthly List of East European Accessions (EEAI), LC, Vol. 8, No. 8, August, 1959. Uncl.

METELKA, J.

The course of learning and forgetting in an electronic model. p. 33.

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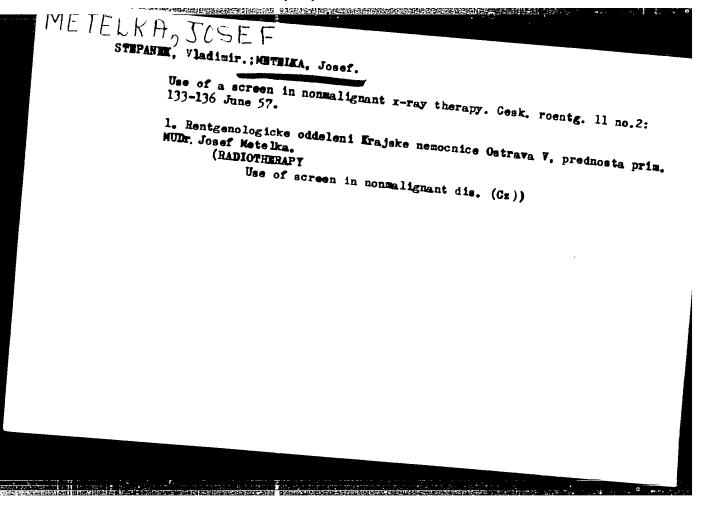
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METELEA, Josef, Dr (Pivovarska 38, Ostrava I)

Roentgenography of the coracoclavicular joint. Lak. listy, Brno 9 no.21:487-489 1 Nov 54.

1. Z ustredniho rtg. oddeleni KUHZ nemocnice Ostrava V. Zabreh, Prednosta Dr Josef Metelka. (SHOULDER, anatomy and histology, coracoclavicular joint, x-ray)

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STEPANEK, Vladimir, Dr. METRIKA, Josef, Dr.

Tomographic & x-ray functional investigation of mandibular joint.

Cesk. rentg. 12 no.1:10-12 Mar 58.

1. Rtg. odd. KUEZ v Ostrave V. prednosta prim. Dr. Jos. Metelka.

V. S. Poskov 61 u Ostravy.

(MANDIBLE, radiography mandibular joint, tomography & x-ray, diag. value (Cz))
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Metelha Josef, Dr.; PINOS, Ladislav, Dr.; METELKA, Josef, Dr.

Gargoylism; 2 cases reports & x-ray aspects. Cesk. rentg. 12 no.1: 24-28 Har 58.

1. Rentgenologicke oddeleni KUNZ v Ostrave-Zabrehu, prednosta primar MUDr Josef Metelka. V. S. Paskov 61 u Ostravy. (LIPOCHONDRODYSTROPHY, manifest. x-ray (Cz))

STEPANEK, Vladimir; METELKA, Josef

Generalized hyperostosis & pachyderma with gastrointestinal hypertrophy.

Gesk. rentg. 12 no.4:246-249 Dec 58.

1. Rtg. odd. KUNI - Ostrava V. V. S., UStr. rtg. odd. nemocnice, Ostrava V. Syllahova 19.

(BONE DISEASES, case reports
pachyperiosteoderma with gastrointestinal hypertrophy (Cz))

(SKIN DISEASES, case reports
same)

(GASTROINTESTINAL DISEASES, case reports
hypertrophy with pachyperiosteoderma (Cz))

STEPANEK, Vladimir; METELKA, Josef

Fragilitas Essentialis Ossium. Cesk. pediat. 14 no.2:134-137 5 Feb 59.

1. Rtg. odd. KUNE v Ostrave, prim. dr. Josef Metelka. V. S., Paskov ol u Ostravy.

(OSTEOGENESIS IMPERFECTA, case reports fragilitas essentialis ossium (C7))

STEPANEK, Vladimir; METELKA, Josef.

Our experiences with grid-roentgenotherapy of non-neoplastic diseases. Cesk. rentg. 14 no.1:5-6 F \*60.

1. Rtg odd. KUNZ v Ostrave V, prednosta prim. dr. Jos. Metelka. (RADIOTHERAPY)

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acific trade in the second CEPEK, Edenek, MUDr; METELKA, Miroslav, MUDr PROPERTY OF THE PROPERTY OF THE PARTY OF THE Treatment of intestinal obstruction. Roshl.chir. 34 no.6:339-351 June 55. 1. OUNZ Jindrichuw Hradec, chirurgicke oddeleni-prednosta prim. MUDr Zdenek Cepek (INTESTINAL OBSTRUCTION pathol. & surg.)

CEPEK, Zdenek, MUDr.; METEIKA, Miroslav, MUDr.

Volvulus of mesogaster with incomplete rotation of the intestines in 18-year-old girl. Heshl. chir. Jo no. J:131-136 Mar 57.

1. OUNZ Jindrichuv Hradec, chir. oddeleni, prednosta MUDr Zdenek Cepek.

(INTESTINAL OBSTRUCTION, case report

volvulus of mesogaster with incomplete rotation (Cz))

# CEPEK, Z.; METELKA, M. Clucocorticoids in the prevention of adhesive ileitis. Cesk. gastroent. vyz. 15 no.5:342-347 Ag '61. 1. Chirurgicke odd, OUNZ Jindr. Hradec, prednosta prim. dr Z. Cepek. (ILEITIS prevent control) (ADRENAL CORTEX PRONES ther)

METELKA, M.; SKALA, E.; FUCHSOVA, M.

Pasting of severing peripheral nerves with plasma coagulum. Rozhl. chir. 41 no.12:802-809 D '62.

1. Neurochirurgicka klinika fak. vseob. lek. University Karlovy v Praze, prednosta prof. dr. Z. Kunc Transfuzni oddeleni UVN v Praze, prednosta MJDr. E. Skala Patologickanatomicke oddeleni UVN v Praze, prednosta MUDr. M. Vorreith. (PERIPHERAL NERVE DISEASES) (PLASMA)

CIA-RDP86-00513R001033710020-4"

**APPROVED FOR RELEASE: 07/19/2001** 

METELKA, M.; MALY, Z.

Arachnoid cysts of the brain. Rozhl. chir. 43 no.10;663-667 0 '64.

1. Neurochirurgicka klinika fakulty vseobechneho lekarstvi Karlovy University v Praze, (prednosta prof. dr. Z Kunc, DrSc.).

	AP6005651 SOURCE CODE: CZ/0079/65/007/002/0160/0161 55 44,55 Ehrlich, V.; Hetelka, M.; Vanickova, M.
ORG: L	stitute of Hygiene, Prague; Neurosurgical Department, Medical School, 55 I
potentia Interdia	Final modification of our method of implanting electrodes for recording ls from deep CRS structures [This paper was presented at the Third 4455 ciplimary Conference on Experimental and Clinical Study of Higher Nervous s held in Marianske Lasne from 19 to 23 October 1964.]
	Activitas nervosa superior, v. 7, no. 2, 1965, 160-161
TOPIC T	GS: central nervous system, electrophysiology, electrode
and th	The field of operation can be covered up and healed, and preby infection is eliminated. Silver wire insulated with is fixed to the hole in the skull with Duracryl; close skull the wire is bare and is bent caudally and fastened.
with a	side of the body are contained in a PVC tube. The PVC
with a and out	Silver wire to the crista. Leads are fixed to the crista
with a and out tube 1	side of the body are contained in a PVC tubes The PVC contained in a silicon tube which is inert to the tissue.
with a and out tube 1	side of the body are contained in a PVC tube. The PVC

VLADYKOVA, J.; METELKA, M.; VLADYKA, V.

Post-traumatic cortical blindness. Cesk. oftal. 21 no.6:
497-502 N '65.

1. Ocni oddeleni UVN v Praze (vedouci doc. dr. V. Jensi),
Neurochirurgicka klinika fakulty vseobecneho lekarstvi
Karlovy University v Praze (prednosta prof. dr. Z. Kunc,
DrSc.).

METELKA, M.

Surgical introgenic lesions of peripheral nerves. Rozhl. chir. 44 no.9:614-619 3 165.

Water Company of the Company of the

1. Neurochirurgicka klinika fakulty vseobecneho lekarstvi Karlovy University v Praze (prednosta prof. ir. Z. Kunc, DrSc.).

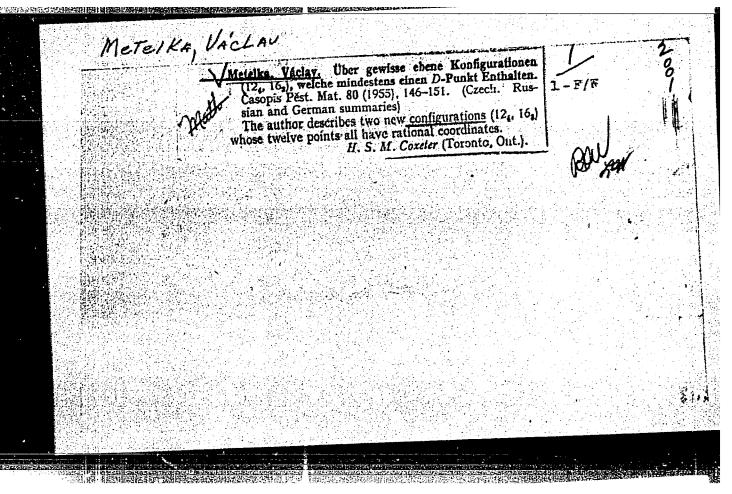
### CZECHOSLOVAKIA

METELKA, M.; Neurosurgical Clinic, Faculty of General Medicine, Charles University (Neurochirurgicka Klinika Fakulty Vseobecneho Lekarstvi KU), Prague, Head (Prednosta) Prof Dr Z. KUNC.

"Anastomosis of the 7th and 12th Nerves Using Plasma."

Prague, <u>Ceskoslovenska Neurologie</u>, Vol 29, No 5, Sep 66, pp 305 - 310

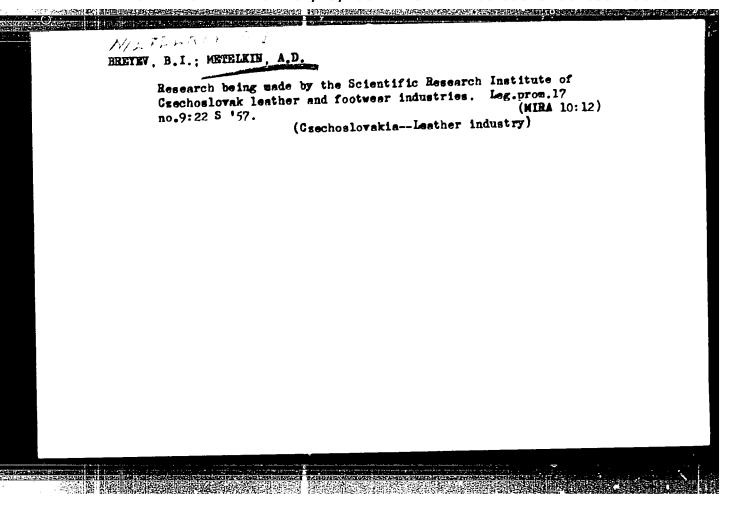
Abstract /Author's English summary modified 7: A group of 26 patients with anastomosis of the 7th and 12th nerves by nerve suture was compared to a group of 36 patients in whom anastomosis was made by autologous plasma. The latter method gives better results, by autologous plasma. The latter method gives better results, mainly in voluntary and emotional movements of facial muscles; the loss of axons is reduced. Full functional recovery cannot be achieved by crossed anastomosis; best results are obtained in an anastomosis of the interrupted nerve in the posterior fosma. The case of 2 patients is discussed; the degree of recovery of the functions of facial muscles depends not only on the technique of surgery, but also on long-term rehabilitation. 4 Figures, 3 West-

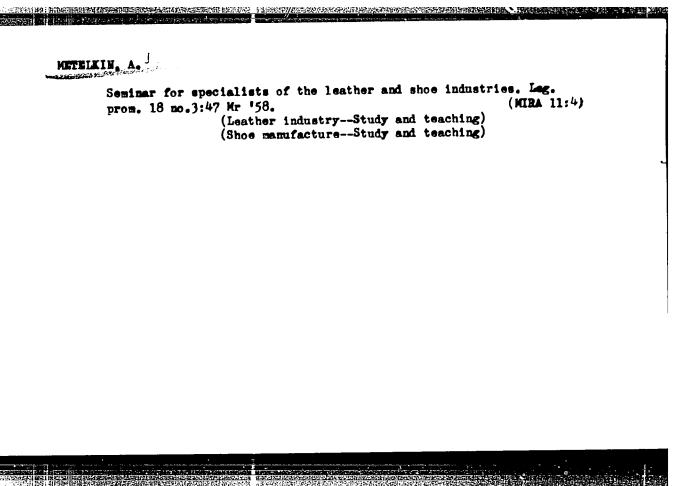


METELKIN, A., prof. (Moskva); METELKIN, O. (Moskva)

Reviews and discussions. Izv. AN Kezakh. SSE. Jer. biol. (MIRA 18:12)

nauk 3 no. il 165.

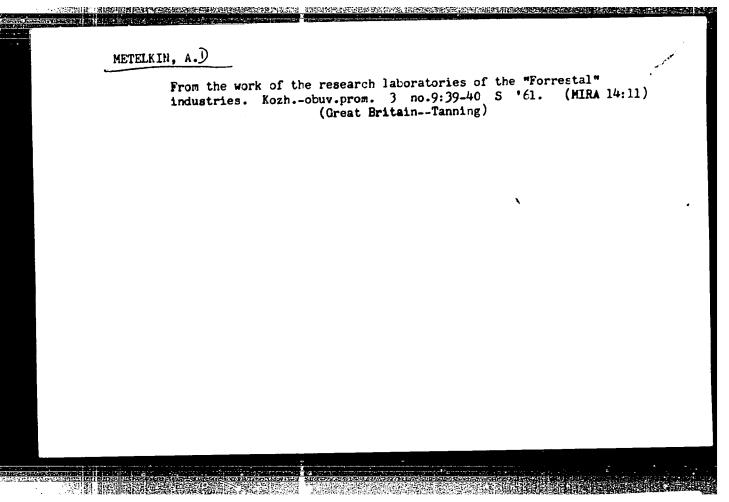




Corn oil instead of castor oil. Prom.koop. 13 no.2:18 F 159.

(MIRA 12:4)

(Leather industry—Equipment and supplies)



### METELRIN, A. F.

Metelkin, A. F. -- "Investigation of the Technological Factors which Influence the Accuracy of the Coupling of Precision Plunger Couplings." Min Higher Education USSR, Moscow Order of Labor Red Banner Higher Technical School imeni Bauman, Moscow 1955 (Dissertation for the Degree of Candidate in Technical Sciences)

SO: Knizhnaya Letopis', No. 23, Moscow, Jun 55, pp 87-104

 On wedging	precision (Pistons)	plunger pair (Fuel pumps)	e. [Trudy]	NVTU no.4	4:9-18 (MIBA 9	•55• 9:6)
	(- Te 40me)	7-2 FE				

122-4-7/29

Metelkin, A.F., Candidate of Technical Sciences. AUTHOR:

The selective assembly of plunger and cylinder pairs. TITLE: (Selektivnaya sborka plunzhernykh par.)

"Vestnik Mashinostroeniya" (Engineering Journal), 1957, No. 4, pp. 40 - 41 (U.S.S.R.) PERIODICAL:

ABSTRACT: The selective assembly of diesel engine fuel pump plungers and cylinders is at present carried out by finding a plunger which enters the cylinder to about 1/3 of its length followed by lapping, which is completed when the plunger enters freely for the whole of its length. The judgment is subjective. The assembly is then inspected to verify its free movement after washing the component in petrol and diesel fuel. The final inspection test consists of measuring the leakage rate of a fine oil under a given piston load. Observations at the Noginsk plant of fuel supply equipment (Noginskiy Zavod Toplivnoy Apparatury) and at the Kharkov Tractor Plant (Kharkovskiy Traktorniy Zavod) KhTZ have revealed the main difficulties of inspection. The precise measurement by a pneumatic comparator is recommended to reduce materially the labour consuming sele-

ction during assembly and the work involved in lapping. There are 2 figures.

AVAILABLE:

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80V/3749

Moscow. Vyssheye tekhnicheskoye uchilishche imeni Baumena

Voprosy tochnosti v mashinostroyenii; [sbornik] Problems of Accuracy in Machine Building; Collection of Articles) Moscow Mashgiz, 1960. 159 p. Errata slip inserted. 5,000 copies printed.

Ed.: V.M. Kovan, Doctor of Technical Sciences, Professor; Ed. of Publishing House: G.I. Baydakov; Tech. Ed.: A.Ya. Tikhanov; Managing Ed. for Literature on Metalworking and Tool Making (Mashgiz): V.V. Rzhavinskiy, Engineer.

PURPOSE: This book is intended for the technical personnel of machine-building plants. It may also be useful to process engineers and scientific workers doing research on the accuracy of machined parts

COVERAGE: In this collection of articles faculty members of the Moscow Higher Technical School imeni Bauman (MVTU) discuss methods of calculating errors connected with setting up workpieces in machine tools. The extent of errors in fastening blanks in three-jaw self-centering chucks is also reviewed. Methods of

Card 1/3

80V/3749 Problems of Accuracy in Machine Building (Cont.) calculating probable inaccuracies in machined parts and magnitude of errors in centerless grinding are discussed. The effect of nonstability of cutting forces on the accuracy of machining, and factors affecting the accuracy of conjugation of precision plunger pairs are discussed. No personalities are mentioned. References follow some of the articles. TABLE OF CONTENTS: Kalinin M.A. [Candidate of Technical Sciences]. Determination of Errors in 5 Holding Work in a Three-jaw Self-Centering Chuck Kapustin, N.M. [Candidate of Technical Sciences]. Machining Accuracy in 17 Centerless Grinding Korsakov, V.S. [Doctor of Technical Sciences]. Effect of the Instability of Cutting Forces on the Accuracy of Machining Metelkin, A.F. [Candidate of Technical Sciences]. Investigation of Factors Affecting the Accuracy of Conjugate Precision Plunger [-Cylinder] Pairs Card 2/3

APPROVED FOR RELEASE: 07/19/2001 CIA-RDP86-00513R001033710020-4"

Problems of Accuracy in Machine Building (Cont.)

Sov/3749

Sasov, V.V. [Candidate of Technical Sciences]. Calculation for Accuracy of Operations in Machining Nonrigid Shafts On Multiple-Tool Machines 121

Solodov, M.D. [Candidate of Technical Sciences]. Calculation of Errors in Centering Affecting the Machining Accuracy of Shafts 145

AVAILABLE: Library of Congress

WK/rn/gap
Card 3/3

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84356 \$/191/60/000/008/008/014 B004/B056

AUTHOR:

Metelkin, A. F.

TITLE:

Use of Epoxy Resins for Assembling Machine Pa ts

PERIODICAL:

Plasticheskiye massy, 1960, No. 8, pp. 34-39

TEXT: At the laboratory of the Kafedra "Tekhnologiya mashinostroyeniya" MVTU im. Baumana (Chair of Mechanical Engineering, Moscow Higher Technical School imeni Bauman), the usability of epoxy resins for connecting machine parts was investigated. Dowel joints (Figs. 1 and 4) were subjected to tensile and torsional tests, and tube connections (Figs. 2, 3, 5) were subjected to tensile and density tests. The loading methods are outlined in Fig. 6. As 54-2 (BF-2) and 54-4 (BF-4) glues did not give satisfactory results, the first of the epoxy resins 3A-5 (ED-5) and 3A-6 (ED-6) was used. Maleic anhydride, polyethylene polyamide, and hexamethylene diamine were used as hardeners. 150 - 160°C was found to be the optimum temperature for hardening. From Fig. 8, the following values of the breaking load at this temperature were found: with 20% hexamethylene diamine, about 2800 kg; with 30% maleic anhydride, about 3000 kg; and Card 1/3

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Use of Epoxy Resins for Assembling Machine Parts

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with 8% polyethylene polyamide, about 2600 kg. At a lower content of polyethylene polyamide, values up to 3200 kg could be obtained (Fig. 7), but in this case the resin becomes so thick that pouring into narrow clearances is made difficult. Fig. 9 shows that the optimum duration of heating for maleic anhydride is 30 min, and for the two other hardeners it is 60 min. Without heat treatment (in construction work or in the case of very large machine parts), hexamethylene diamine or polyethylene polyamide may be used. It follows from Fig. 10 that the greatest breaking load was obtained at 0.2 - 0.3 mm clearance. The dowel joints withstood the torsional moment (up to 700 - 1300 kg·cm) during the tightening of screws. Fig. 11 shows the dependence of the breaking load on the clearance in the case of thin-walled tubes: Optimum at 0.05 - 0.1 mm. In the case of gas- and water-pipes, 1 to 2 mm clearance gave sufficient strength. In this case, Viniplast powder, foundry dust, quartz sand, cement, metal shavings, and metal powder were used as fillers. The latter gave the best results; but also with 50% quartz sand, the breaking load was not below 1500 kg. 3/4 and 1 3/4 inch tubes gave a breaking load of 2800 to 3000 kg with ED-5 and hexamethylene diamine. The tubes remained tight at 10 atm. Repeated heating of hot-hardened tube connections (Fig. 12) at 100°C caused the breaking load to decrease, but this remained within the Card 2/3

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Use of Epoxy Resins for Assembling Machine Parts

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permissible limits. Cold-hardened tube connections did not withstand this test. Cooling down to -70°C was without influence upon strength. The author discusses the reduction of expenses by using resin to be expected as a result of the elimination of surface treatment and thread-cutting. The material costs for resin are 3 kopecks per dowel joint, and for a connection of thin-walled tubes 12 kopecks. Mention is made of the luting of bicycle frames at the "Mifa" works in Eastern Germany. There are 12 figures and 1 Soviet reference.

Card 3/3

APPROVED FOR RELEASE: 07/19/2001 CIA-RDP86-00513R001033710020-4"

METRIKIE, A.F.; KARPOVA, K.A., inshener; LUR'YE, L.S., kandidat tekhnicheskikh nauk; KYAZIN-ZADE, RAUK; HAKHINOV, G.R., detsent, kandidat tekhnicheskikh nauk; KYAZIN-ZADE, Z.I., detsent, kandidat tekhnicheskikh nauk.

Remarks on the textbook on theoretical electric engineering for higher (NLRA 6:11) achoels. Blektrichestve mo.12:70-72 D '53.

1. Ivanovskiy energeticheskiy institut im. Lemina (for Netelkin and Karpova).
2. Vseseyusmyy nauchne-issledovatel'skiy institut elektrifikatsii sel'skoge
2. Kseseyusmyy nauchne-issledovatel'skiy institut im. Asisbekova (for khesyaystva (for kur'ye). 3. Sredneasiatskiy pelitekhnicheskiy imstitut im. Asisbekova (for kur'ye).
3. Kseseyusmyy institut im. Asisbekova (for kur'ye).

(Electric engineering--Textbooks)
(Electric engineering--Textbooks)

MITELKIN, A.F., (Ivanovo); LYUBIMOV, M.A., (Ivanovo).

Experiments with a cathode tube to explain the principle of electric current. Fiz.v shkole 13 no.3:63-65 My-Je '53.

(Gathode ray tubes) (Electric currents)

Study of electric spark discharges. Fiz.v shkole 14 no.2:52-54

Mr-Ap '54.

1. Gorod Ivanovo, Energeticheskiy institut im. V.I.Lenina.

(Electric discharges through gases) (Electrophorus)

METELKIN, A.F.

GRUSHEVSKIY, B.V., dotsent, kandidat tekhnicheskikh nauk; KONSTANTINOV, V.I., inzhener (Moscow); METEIKIN, A.F.; LTUBIMOV, M.A.; TABACHINSKIY, V.F., dotsent, kandidat tekhnicheskikh nauk; BOZAKOV, S.P., professor, doktor tekhnicheskikh nauk; LAVROV, V.M., dotsent, kandidat tekhnicheskikh nauk; ERON, O.B., professor, doktor tekhnicheskikh nauk (Lenningrad).

The field as an aspect of matter. Elektrichestvo no.2:55-64 F-55. (MIRA 8:2)

1. Donetskiy industrial'nyy institut (for Grushevskiy). 2. Ivanovskiy energeticheskiy institut im. Lenina (for Metelkin and Lyubimov).
3. Kafedra teoreticheskikh osnov elektrotekhniki Leningradskogo instituta inzhenerov zheleznodorozhnogo transporta (for Tabachinskiy).
4. Kafedra elektrooborudovaniya MIKhM (for Rozanov). 5. Moskovskiy elektrotekhnicheskiy institut svyazi (for Lavrov).

### "APPROVED FOR RELEASE: 07/19/2001 CIA-RDP86-00513R001033710020-4 THE STATE OF THE S

METELKIN, A.F.

AID P - 1463

Subject

: USSR/Electricity

Card 1/1

Pub. 27 - 14/36

Author

Metelkin, A. F. and Lyubimov, M. A.

The field as an aspect of matter (Discussion of the

Title

article by O. B. Bron, Elektrichestvo, No. 7, 1954)

Elektrichestvo, 2, 57, F 1955 Periodical:

Abstract

The author agrees in principle with the approach of O. B. Bron, but criticizes some of his presentations,

as, for example, the nature of heat which is presented as substance and in other places as field.

Institution:

Ivanov Power Engineering Institute im. Lenin

Submitted :

Grant Company of the company of the

No date

METELKIN, AF.

AID P - 2361

Subject

: USSR/Electricity

Card 1/1

Pub. 27 - 25/30

Authors

: Metelkin, A. F. and Lyubimov, M. A.

Title

: A different formula for the Biot-Savart law (Concerning an article by V. M. Yuzhakov in this journal, No.8, 1954)

Periodical: Elektrichestvo, 5, 84-85, My 1955

Abstract

The authors consider that V. M. Yuzhakov did not present any "different" mathematical formulation of the law. This formula results from the usually accepted one. It does not bring anything new in the calculations of field intensity. Two Soviet references (1950-1951).

Institution:

Ivanovsk Power Engineering Institute im. Lenin

Submitted : No date

METELKIN, A.F. (Ivanovo)

Experiments with Franklin's "wheel," Fiz. v shkole 21 (MIRA 14:9) no.1:68 Ja-F '61.

(Cloctricity—Experiments)

ENCT(d)/ENT(1)/ENT(m)/ENP(w)/E	EWA(d)/EPR/EWP(t)/EWP(k)/EWP(b)/EWA(c)
Pf-4 MJH/JD/HH/EM ACCESSION NR: AP5012893	UR/011/5/65/000/001/001/5/00535/6
AUTHORS: Metelkin, A. F. (Candidate of t I. (Aspirant)	echnical sciences, Docent); Pavlov, Yu.
TITLE: Cortain problems of increasing the	ne exploitation safety of pipe connections
SOURCE. TVIZ. Mashinostroyeniye, no. 4	, 1965, 45-53
TOPIC TAGS: pipe flow, joint, stress di calculation, stress relaxation/ KI 961 s	stribution, stress analysis, stress teel, KH18N9T steel
AESTRACT: Stress distribution during th	e work of a pipe-connection under sudden
derived for the axial weakening in the continuous of thread, and for the total	onnection, the radial and axial weakening free play in the junction. Theoretical
prevent the formation of leaks and to end in recommended to eliminate the joints come of lesser thermal stress, or to decome	whom noggible), to transfer them into a
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6 figures and 3 formulas.  ASSOCIATION: Moskovskiy a logical Institute of Aviat	viatsionnyy tekhnologicheskiy	institut (Mos	
6 figures and 3 formulas.	viatsionnyy tekhnologioheskiy ion)	institut (Mos	cow Techno-

L 00914-66 ENT(1)/ENT(m)/ENP(w) JD/EM ACCESSION NR: APS019516 UR/0145/65/000/006/0102 621.6.038 AUTHORS: Matelkin, A. P. (Cardiste of technical eciences, Docent); Pavlov (Aspirant); Mitkin, S. D. (Engineer) TITLE: Streeee in pipes SOURCE: 1902. Mashinostroyeniye, no. 6, 1965, 102-107 TOPIC TAGS: stress load, strain gage, experimental method, static stress, dynamic stress, thermal expension ABSTRACT: The stresses in a pipeline are divided into dynamic and static components E . - Equit Eeen The dynamic stresses are produced by oscillations generated by the flow velocity, pressure, and engine vibrations; the static stresses are caused by thermal expension. To determine these stresses during operation, the hydraulic conduits of three engines were experimentally investigated. The stresses were measured by strain gauges and recorded on oscillograms. The test results show that the hydrosystem pipeline can be divided into three dynamic stress somes corresponding to Cord 1/2 

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stresses not great level in the pipes mounting stresses the mounting stress amount to 19-20 kg as the use of flex connections also h	er then 2.5, 4, and 7 was 200-500 cycles/s in the pipes. Resultises are a direct functible metallic joints have the advantage of	kg/mm² respectively.  sec. A special effort  to of studies on 10 pi ction of construction gested for reducing mo and self-adjusting sy low frequency vibrati to the vibration-indu	pelines indicate the miseligments and counting stresses, such stems. Flexible one. Pressure stressed and the about 10-15 kg/m².	t pld
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AUTHOR: Metelkin, A. F. (Gandidate of technical aciences; Docent); Maylor, Yu. I. (Engineer); Matyachin, L. V. (Engineer)  ORG: Moscow reco. legical aviation institute (Moskovskiy aviatsion), technicheskiy institut)  TITLE: Effect of cleaning methods on fatigue of pipelines of aircraft engine hydraulic systems  SOURCE: IVU7. Mashinestroveniye, no. 6, 1966, 53-56  TOPIC FACS: stainless steel, pipeline, hydraulic system, pipeline, aircraft, hydraulic system; pipeline tatigue strength/Kh18N10T steel  ABSTRACT: Experiments have been made to develop an optimal cleaning method for welded or brazed stainless-steel pipelines of aircraft-engine hydraulic systems. Chemical and ultrasonic pickling in different solutions of sulfurio, hydrochloric, nitric, and hydrofluoric acids at various temperatures were tested. Ultrasonic pickling in and hydrofluoric acids at various temperatures were tested. Solution containing 3Z nitric and 3Z hydrofluoric acids at 18—25C was found to be the solution containing 3Z nitric and 3Z hydrofluoric acids at 18—25C was found to be the solution containing 3Z nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric and 3Z hydrofluoric acids at la—25C was found to be the solution containing at nitric a	٠	SOURCE CODE: UR/0145/66/000/006/0053/0056	
ORG: Moscow recomblegical Aviation Institute (Moskovskiy aviatsion), terinicheskiy institut)  TITLE: Effect of cleaning methods on fatigue of pipelines of aircraft engine hydraulic systems  SOURCE: IVU7. Mashinostroveniye, no. 6, 1966, 53-56  TOPIC FACS: stainless steel pipeline, hydraulic system pipeline, aircraft hydraulic system pipeline fatigue strength/Kh18N10T steel  ABSTRACT: Experiments have been made to develop an optimal cleaning method for welded or brazed stainless-steel pipelines of aircraft-engine hydraulic systems. Chemical and ultrasonic pickling in different solutions of sulfurior, hydrochloric, nitric, and ultrasonic pickling in different solutions of sulfurior hydrochloric, nitric, and hydrofluoric acids at various temperatures were tested. Ultrasonic pickling in a solution containing 37 nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 37 nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing and brazed joints, 20 min. Ultrasonically pickled specimens had a fatigue limit (10·10 <sup>th</sup> cycles) of 8.4 kg/mm² for brazed and 7.2 kg/mm² for welded	,	CC NNI APRILAPRILATE	
ORG: Moscow recomblegical aviation institute (Moskovskiy aviatsion). Technicheskly institut)  TITLE: Effect of cleaning methods on fatigue of pipelines of aircraft engine hydraulic systems  SOURCE: IVU7. Mashinostroveniye, no. 6, 1966, 53-56  TOPIC FAGS: stainless stem, pipeline, hydraulic system, pipeline, aircraft, hydraulic system, pipeline taking strength/Kh18N10T steel  ABSTRACT: Experiments have been made to develop an optimal cleaning method for welded or brazed stainless-steel pipelines of aircraft-engine hydraulic systems. Chemical and ultrasonic pickling in different solutions of sulfurio, hydrochloric, nitric, and hydrofluoric acids at various temperatures were tested. Ultrasonic pickling in and hydrofluoric acids at various temperatures were tested. Ultrasonic pickling in a solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydrofluoric acids at 18—25C was found to be the solution containing 3% nitric and 3% hydroflu	1	JTHOR: Metelkin, A. F. (Candidate of technical aciences; Docent); Pavidy, id. 1.	
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ACC NR: AP6022863 SOURCE CODE: UR/0145/66/000/002/0038/0042	
AUTHOR: Metelkin, A. F. (Candidate of technical sciences, Lecturer); Pavlov, Yu. I. (Graduate Student)	-
ORG: Moscow Aviation Engineering Institute (Moskovskiy aviatsionno-tekhnologicheskiy Institut) $\mathcal{F}\mathcal{L}$	
ORG: Moscow Aviation Engineering institute (No. 1984)  Kiy Institut)  TITLE: Strength of aviation pipeline couplings with brazed nipples  SOURCE: IVUZ. Mashinostroyeniye, no. 2, 1966, 38-42	
TOPIC TAGS: stress analysis, pipeline, hydraulic equipment, turbojet engine, metal joining, stress concentration, fatigue strength	
ABSTRACT: The authors study methods for raising the safety factor of pipelines with brazed hipples in turbojet engine hydraulic systems under variable stresses. The pipelines and nipples in this study were made of Khl8N9I steel and brazed by high requency current and oxyacetylene torches using PZh45-81 high-temperature solder. Such joints can withstand pressures of more than 500 kg/cm² and uniform heating up to such joints can withstand pressures of more than 500 kg/cm² and uniform heating up to such joints can withstand pressures of union can function under extreme vibra-	( to
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for calculating the safety factor of pipelines used under variable load conditions. This is based on the fact that variable loads change according to an asymptotic law. In finishing pipeline systems, a safety factor of at least 1.3-1.4 is desirable. In finishing pipeline systems, a safety factor of at least 1.3-1.4 is desirable. This can be achieved by decreasing variable stresses and lowering the static component of normal stresses thus raising the fatigue limit. Tests show that the fatigue limits are approximately the same in pipeline bending for tubes with internal fluid pressure of 100 kg/cm² and atmospheric pressure. The fatigue limit of pipelines is a function of the absolute dimensions of pipe cross section and local stress concentrators. It is shown that the experimental method is most accurate in determining the fatigue limit of pipelines. Data are given for fatigue limits of various diameter pipelines and experimental coefficients of stress concentration for nipples. The minimum safety factor used for existing turbine engine pipelines is 1.75-2.5. The minimum safety factor used for existing turbine engine pipelines is 1.75-2.5. The main problem to be solved is that higher safety factor values should not be accompanied by increased weight and reduced efficiency of the system. Orig. art. has:

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ACC NR: AMG030648

Monograph

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Gevorkyan, Ashot Mushegovich; Ivanov, Andrey Pavlovich; Metelkin, Aleksandr Fedorovich; Moskalev, Mikhail Aleksandrovich

Technology of aircraft engine construction; a manual for thesis writers (Tekhnologiya aviadvigatelestroyeniya; uchebnoye posobiye po diplomnomu proyektirovaniyu)

Moscow, Izd-vo "Mashinostroyeniye", 1966. 174 p. illus., biblio., tables. 9200

copies printed. Textbook for students at aviation schools and faculties.

TOPIC TAGS: aircraft engine, production, production engineering, industrial management

PURPOSE AND COVERAGE: The book is intended for students writing theses on aircraft engine technology, for teaching staffs in aviation institutes, and for production engineers. It can also be useful to other machine building specialities. A systematic presentation is given on the planning of thesis writing on aircraft engine production, production management, introduction of new methods, new machinery, quality control, production automation, and equipment replacement and repair. Included as appendices are several tables dealing with production control and production management. There are 36 references, all Soviet.

Card 1/2

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· ·	and defense of the thesis - 143	
Appendices - 147		
References - 172		
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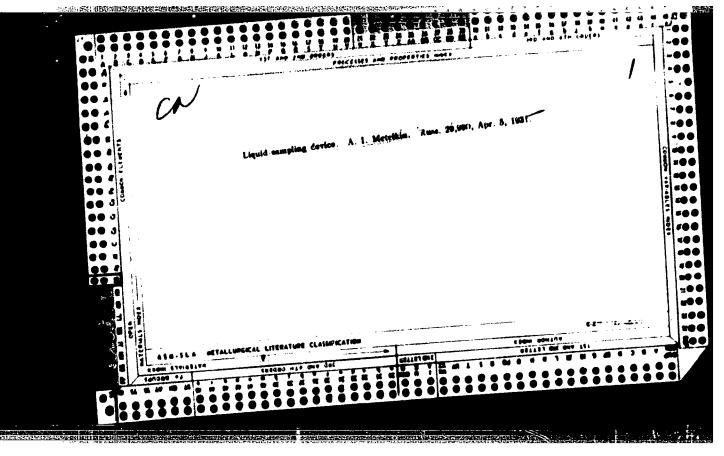
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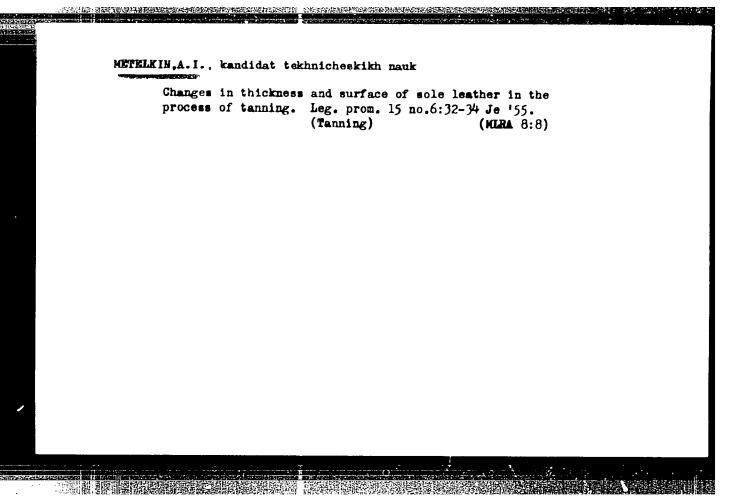
A fuller utilization of tanning agents in the process of tanning.

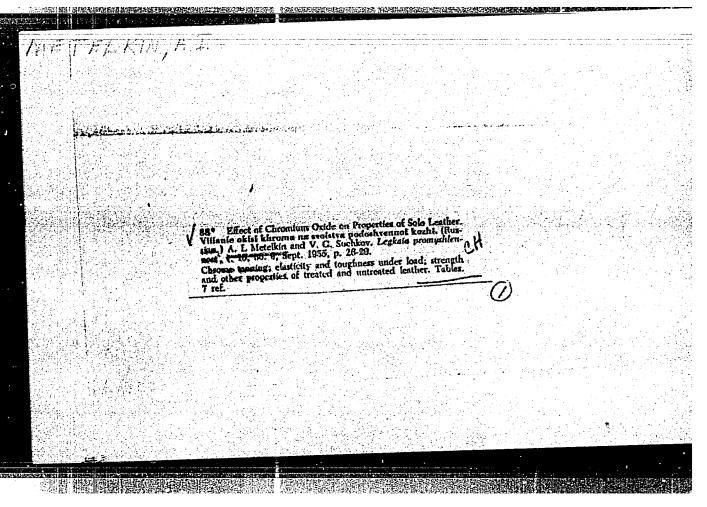
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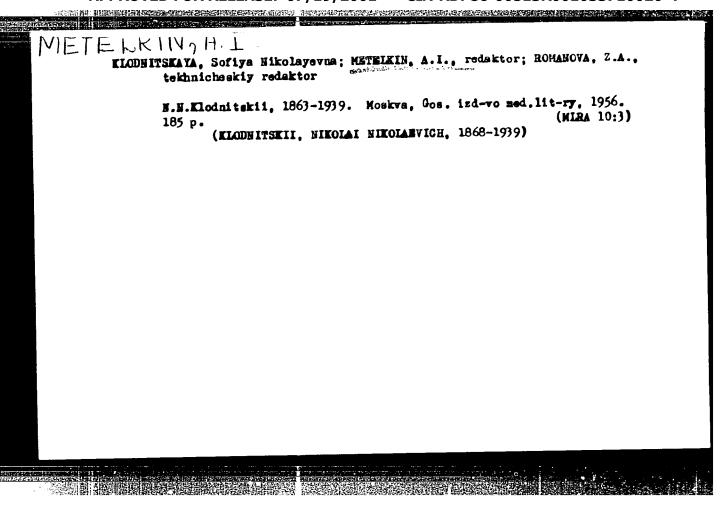
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